Harbour resonance Under long bound waves attack



Layout of the presentation

Harbour resonance



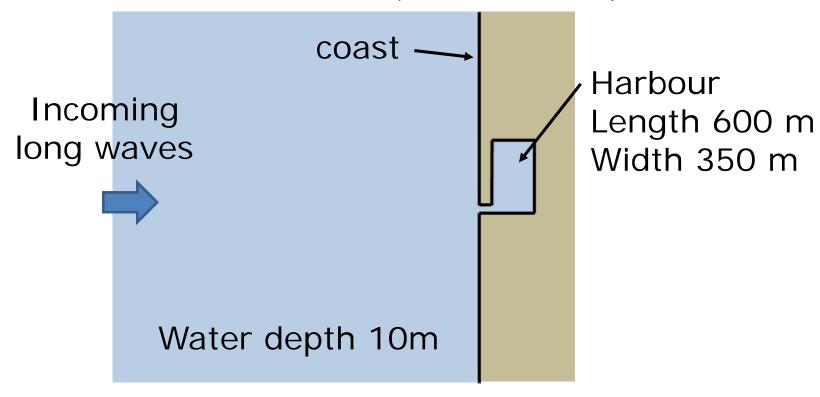
- Long waves
- Study case: the Marina di Carrara harbour
- Numerical modelling of harbour resonance (two methods)
- Conclusions

Sheltering from short (wind) waves

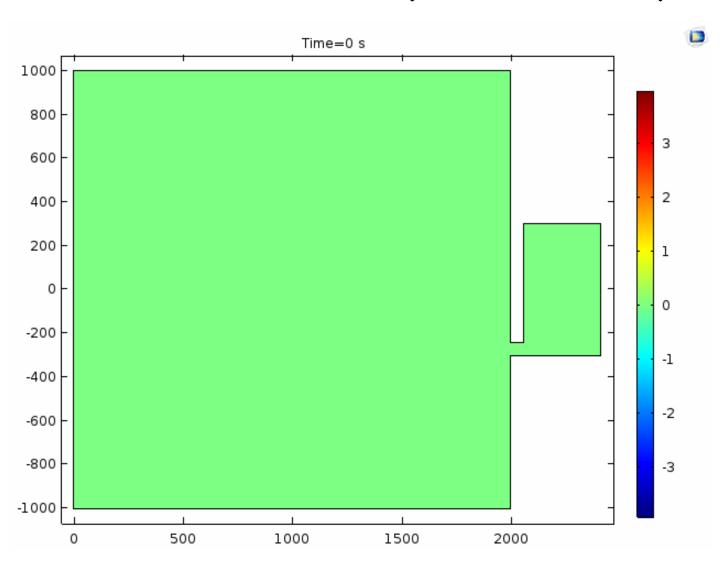


Two example computations: a simple rectangular harbour with entrance at a fully reflective coast. Two long waves periods (T) are selected, representing:

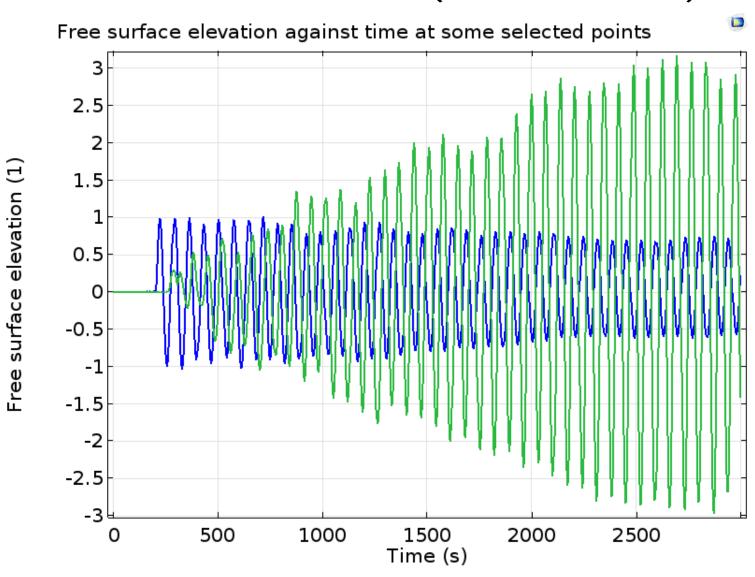
- Resonant condition (T=69.6638 s)
- Non resonant condition (T=80.0000 s)



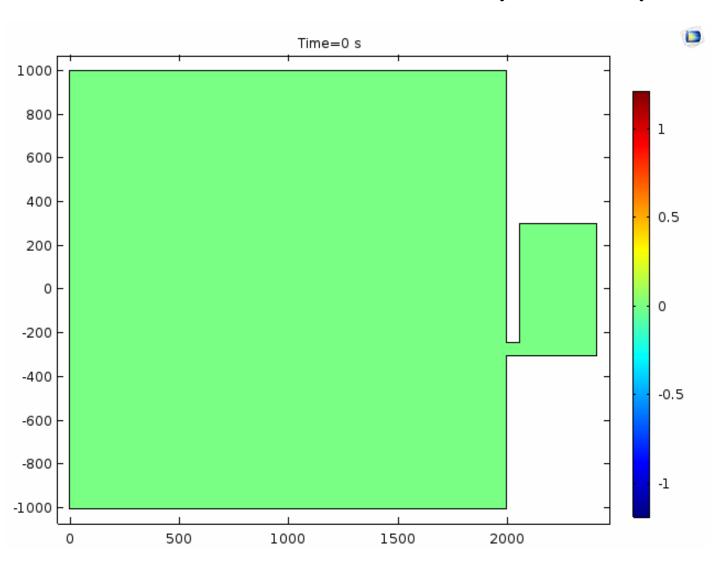
Resonant condition (T=69.6638 s)



Resonant condition (T=69.6638 s)



Non resonant condition (T=80 s)



When the length of the incoming long waves is similar to the length of the waves 'trapped' inside the harbour, i.e. to the natural modes of free surface oscillation.

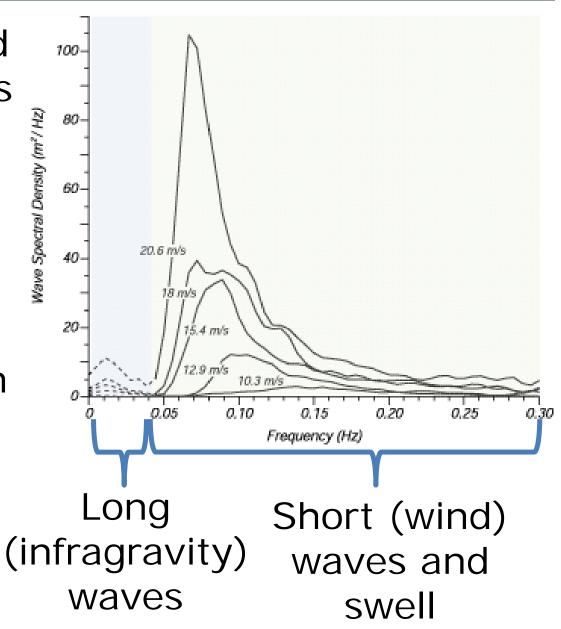
Under these conditions the long waves energy accumulates (is trapped) inside the harbour, leading to large free surface oscillations.

This does not happen with short waves, as their length and period are much smaller than the natural ones of typical harbours.

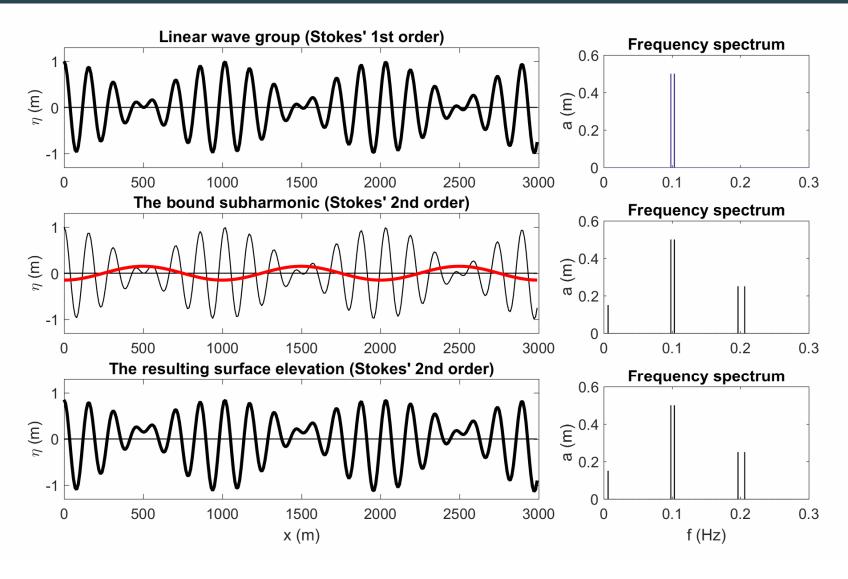
Long waves, where they come from?

They are generated by nonlinear effects when short waves become large and steep.

Also in the surf zone the breaking of wave groups can generate long waves, i.e. surf beats.



Long waves generated by nonlinear interactions



This is an example of LONG bound wave

Long waves generated by nonlinear interactions

- Many sources of data are available for <u>short</u> <u>waves</u> (buoys, satellites, hindcast database)
- No measurement networks for long waves...
- The long waves properties are to be calculated from the short waves
- Need of calculation methods/models

Harbour resonance and long waves

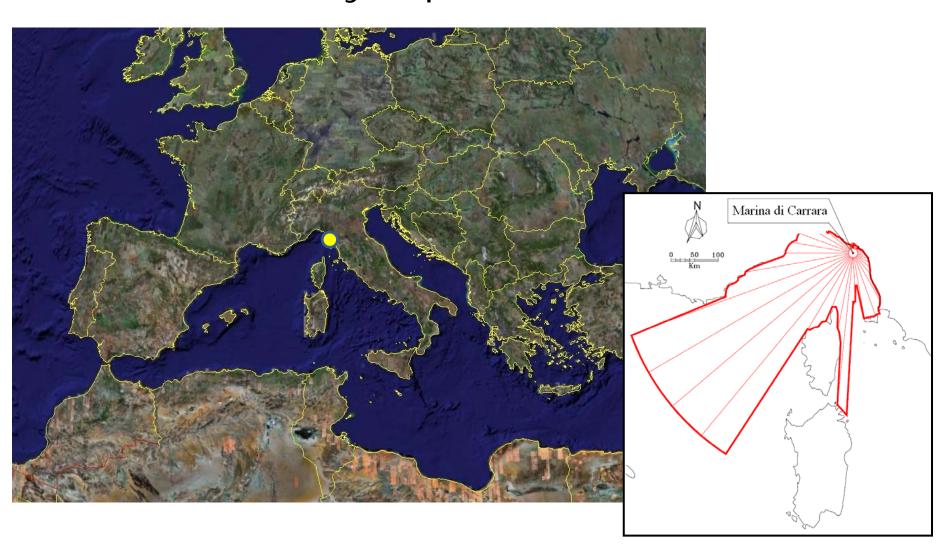
- Long waves are generated by short (wind) waves as they approach to the coast
- Long waves, T=O(100-1000s) can resonate into harbours
- The long waves amplification can lead to harbour operational problems: large oscillations of the moored ships, large forces (breaking) in the mooring lines
- To be carefully addressed during the (first stages of the) design and the management of harbours

Study case: the Marina di Carrara harbour



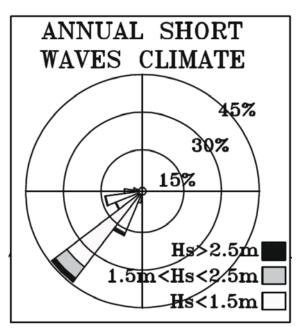
Study case: the Marina di Carrara harbour

The site is mainly exposed from S-SW waves

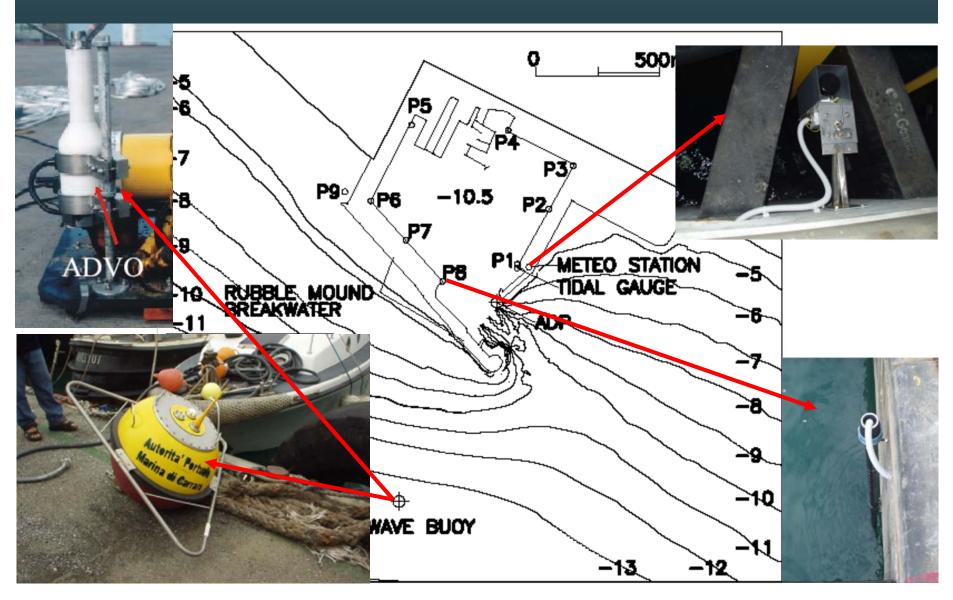


Study case: the Marina di Carrara harbour

The harbor has a rectangular plan-shape with a total surface of 362.000m², a water depth of 10.5m in the dredged basin and a total quay length of 1.650m.







SHORT waves climate in percentage of available measurements outside the harbor

Dec 2005->Oct 2008

H_{m0} range	0-0.5	0.5-1.0	1.0-1.5	1.5-2.0	2.0-2.5	2.5-3.0	3.0-3.5	3.5-4.0	4.0-4.5	>4.5
$2 < T_p \le 2.5$	1.6	-	-	-	-	-	-	-	-	-
$2.5 < T_p \le 3$	10.4	0.3	-	-	-	-	-	-	-	-
$3 < T_p \le 3.5$	18.8	2.3	-	-	-	-	-	-	-	-
$3.5 < T_p \le 4$	12.6	3.9	0.3	-	-	-	-	-	-	-
$4 < T_p \le 4.5$	6.6	4.8	1.6	0.2	-	-	-	-	-	-
$4.5 < T_p \le 5$	4.6	3.8	2.5	1.0	-	-	-	-	-	-
$5 < T_p \le 5.5$	2.1	2.6	2.2	1.2	0.3	-	-	-	-	-
$5.5 < T_p \le 6$	1.2	2.2	1.4	1.1	0.9	0.2	-	-	-	-
$6 < T_p \le 6.5$	0.3	1.2	1.0	0.6	0.6	0.5	0.2	-	-	-
$6.5 < T_p \le 7$	0.1	0.5	0.5	0.5	0.4	0.3	0.3	0.1	-	-
$7 < T_p \le 7.5$	-	0.2	0.2	0.2	0.2	0.1	0.1	0.2	0.2	-
$7.5 < T_p \le 8$	-	0.1	0.1	0.1	-	0.1	-	-	-	0.1

The pressure gauges acquire 24h long bursts at 2 Hz.

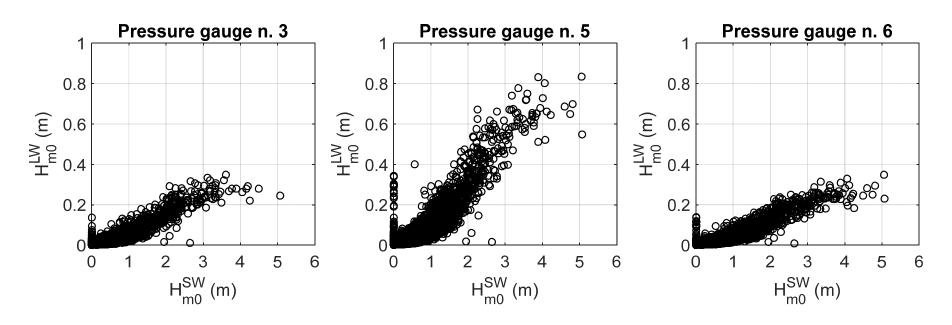
Data have been further divided into 2 hours records and processed by separating:

- very long waves (VLW), f < 0.003 Hz (T>333 s)
- long waves (LW), 0.003
 f < 0.030 Hz (33<T<333 s)

For each frequency band a significant wave height was calculated by integrating the energy density over the appropriate frequencies.

Result: bi-hourly time series of long waves (at the pressure gauges) and incoming short waves (at the buoy) for almost three years.

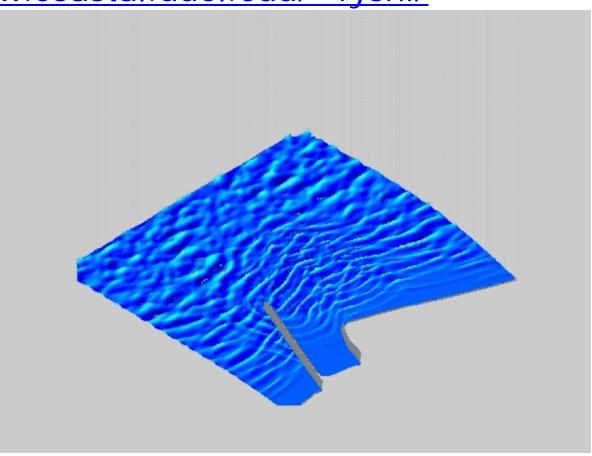
Measured LW height against measured SW height



$$\frac{\text{LW height inside the harbour}}{\text{incoming SW height}} = 0.1 \div 0.2$$

Example result from Prof. Fengyan Shi (University of Delaware, USA)

http://www.coastal.udel.edu/~fyshi/



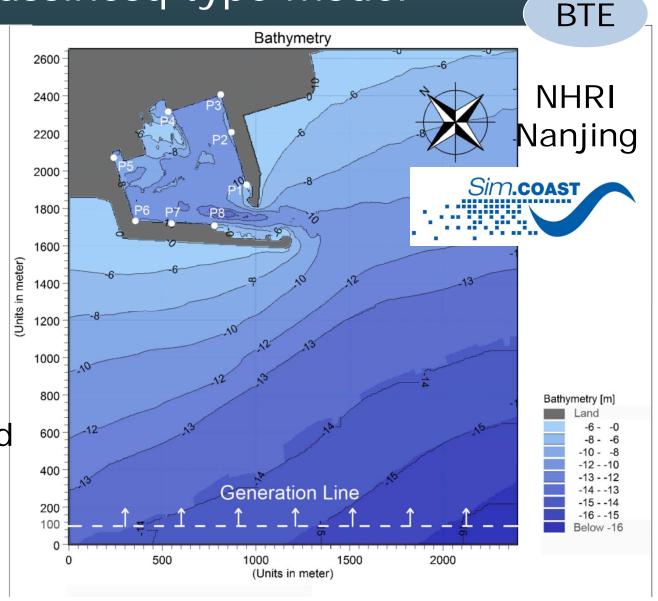
BTE

BTE

Nonlinear numerical models for <u>short and long</u> <u>waves</u> (Boussinesq Type Models)

- reproduce the short waves propagation considering the nonlinear effects: they also model the growth of the long waves.
- The penetration into harbours of both short and long waves is well reproduced including resonance.
- Drawback: high computational costs

- MIKE 21 DHI model has been applied
- Computational domain:
 2395 m x 2650 m, dx=dy=5m
- Unidirectional <u>random</u> short waves generated at the SW boundary
- Long runs



BTE

Short waves climate outside the harbour

H_{m0} range	0-0.5	0.5-1.0	1.0-1.5	1.5-2.0	2.0-2.5	2.5-3.0	3.0-3.5	3.5-4.0	4.0-4.5	>4.5
$2 < T_p \le 2.5$	1.6	-	-	-	-	-	-	-	-	-
$2.5 < T_p \le 3$	10.4	0.3	-	-	-	-	-	-	-	-
$3 < T_p \le 3.5$	18.8	2.3	-	-	-	-	-	-	-	-
$3.5 < T_p \le 4$	12.6	3.9	0.3	-	-	-	-	-	-	-
$4 < T_p \le 4.5$	6.6	4.8	1.6	0.2	-	-	-	-	-	-
$4.5 < T_p \le 5$	4.6	3.8	2.5	1.0	-	-	-	-	-	-
$5 < T_n \le 5.5$	2.1	2.6	2.2	1.2	0.3	-	-	-	-	-
$5.5 < T_p \le 6$	1.2	2.2	1.4	1.1	0.9	0.2	-	-	-	-
$6 < T_p \le 6.5$	0.3	1.2	1.0	0.6	0.6	0.5	0.2	-	-	-
$6.5 < T_p \le 7$	0.1	0.5	0.5	0.5	0.4	0.3	0.3	0.1	-	-
$7 < T_p \le 7.5$	-	0.2	0.2	0.2	0.2	0.1	0.1	0.2	0.2	-
$7.5 < T_p \le 8$	-	0.1	0.1	0.1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.1	-	-	-	0.1

Only 22 selected sea states are reproduced

For each computation the LONG waves at the 8 pressure transducers is calculated

Modelling harbour resonance with the linear model (Mild Slope Equation)

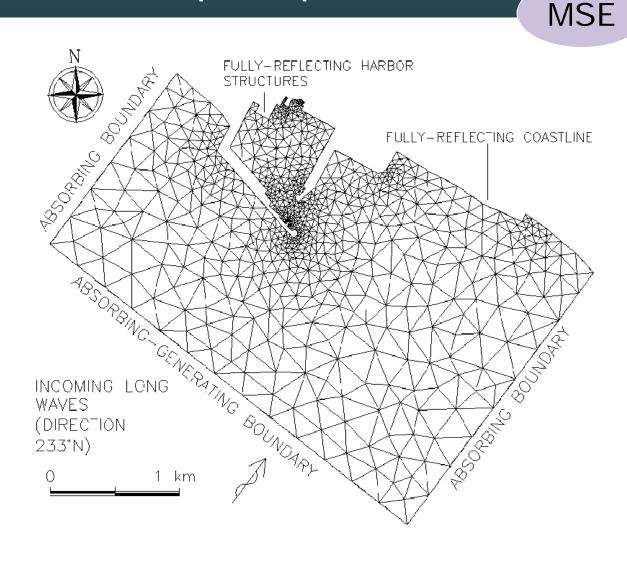
MSE

- Linear models can be applied to predict the long waves amplification inside the harbour
- The LONG waves height can be predicted using the Bowers (1992) formula on the basis of the short waves properties

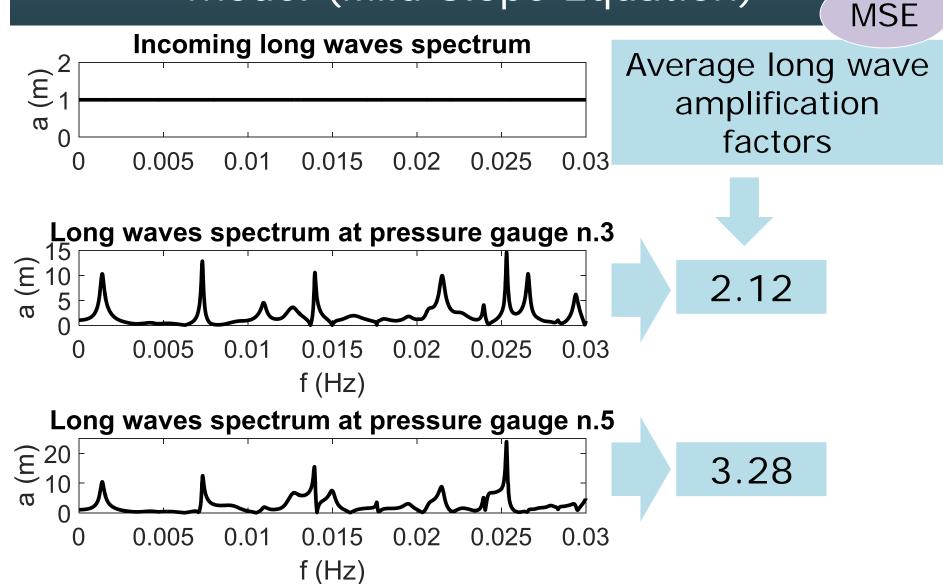
LONG WAVES Hs
$$LWH_{S_i} = k \frac{H_s^{\alpha} T_p^{\beta}}{d^{\gamma}} \quad \text{SHORT WAVES significant wave height}$$
 SHORT WAVES peak period water depth

Modelling harbour resonance with the linear model (Mild Slope Equation)

A linear MSE model is applied to reproduce the long waves propagation and amplification



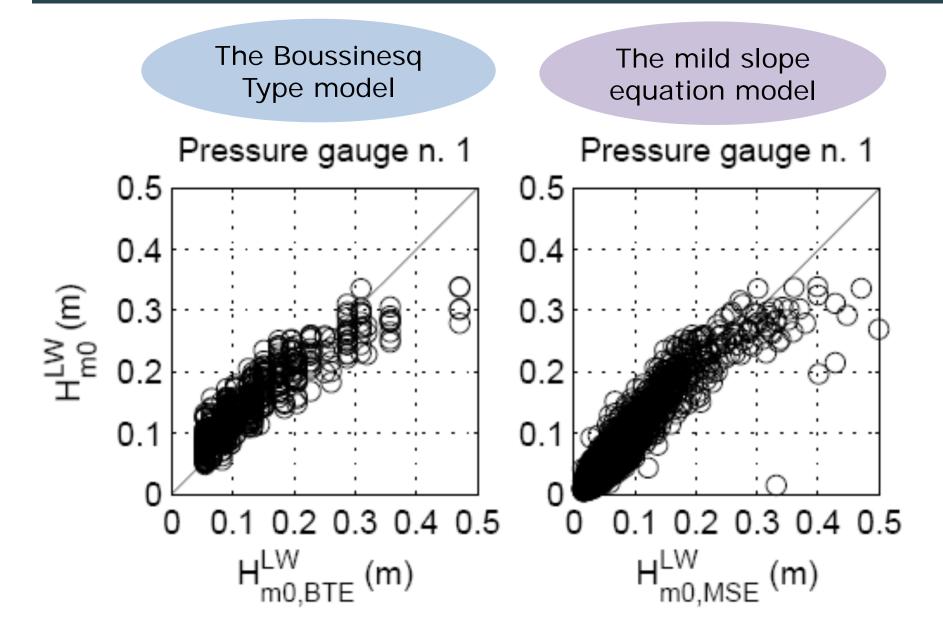
Modelling harbour resonance with the linear model (Mild Slope Equation)



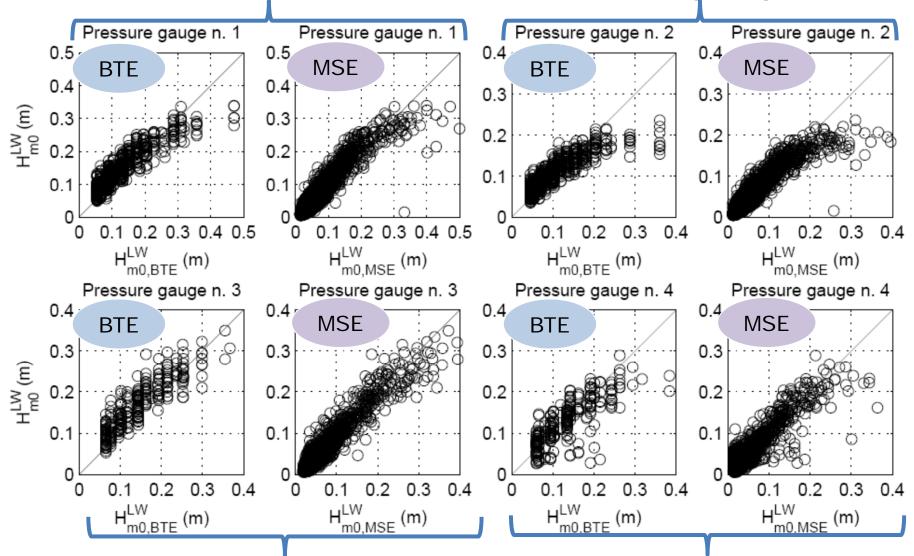
For each recorded sea state are available:

- The long waves height at the 8 pressure transducers (measurements)
- The long waves height at the 8 pressure transducers predicted by method 1 (BTE)
- The long waves height at the 8 pressure transducers predicted by method 2 (MSE)

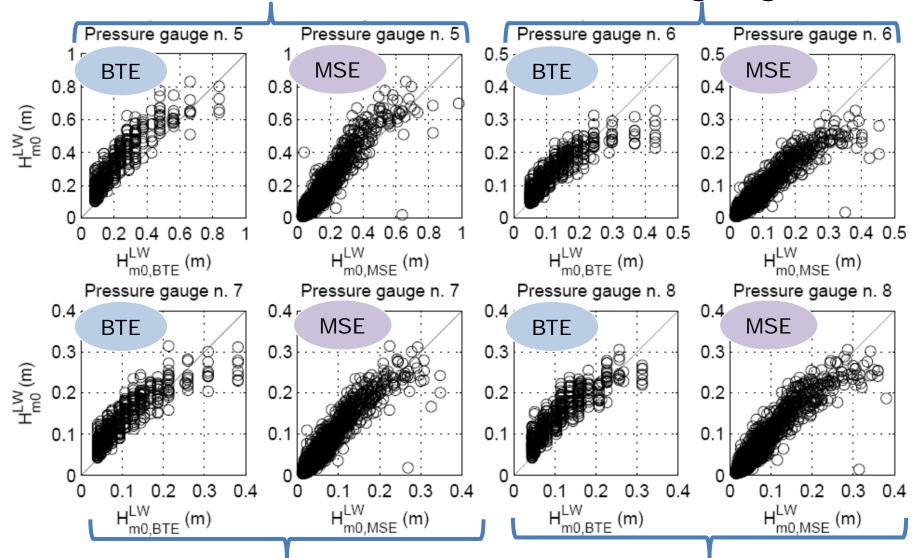
Let us compare BTE and MSE results against measurements.



Pressure gauge n.1 Pressure gauge n.2



Pressure gauge n.5 Pressure gauge n.6



Conclusions

- Measurements of harbour resonance have been presented for the Marina di Carrara harbour
- Two alternative/complementary approaches for the numerical modelling of harbor resonance have been evaluated
- The BTE model has the advantage that a very detailed reproduction of the nearshore flows is obtained, but it is computationally demanding
- The MSE model is computationally cheap, but the incoming long waves must be specified apriori
- Harbour resonance can be very relevant and should be carefully addressed at all stages of engineering design, especially at early stages.